

# Characterization and Determination of the Electrochemical Parameters of EC<sub>irr</sub> Process Via Convolution Voltammetry Combined with Digital Simulation Method

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*Convolution-deconvolution voltammetry was applied to provide a simple and accurate method for characterization the nature of electrode reaction as well as determination of the homogeneous chemical rate constant  $k_c$  and the standard reduction potential  $E^0$  of the EC<sub>irr</sub> mechanism. The experimental data were combined with digital simulation to confirm the nature of electrode reaction and verification of the experimental electrochemical parameters.*

*Keywords: electrochemical parameters, convolution-deconvolution, EC<sub>irr</sub> system, digital simulation*

Convolution-deconvolution voltammetry treatments were considered to overcome the limitation arising from the cyclic voltammetry measurements irrespective of the rate of electron transfer [1-7]. The convolution theorem finds use in the situation where it is required to perform the inverse transformation on a function which is the product of two functions of the Laplace variable each of which individually had known inverse transformations. In such a situation, the convolution theorem gives [8]

$$L^{-1} [f_s(s).g_s(s)] = \int_0^t G(u)F(t-u)du \quad (1)$$

in which  $f_s, g_s$  are the Laplace transform of the functions  $F$  and  $G$ , the variables  $u$  is a dummy variable which is lost when the definite integral is evaluated.

For the following reaction, in which a given species undergoing only electron transfer



and no subsequent processes other than 'linear' diffusion out in the solution from a planar electrode, i.e. the Fick's Second Law is expressed as [9]

$$[\partial C_{Ox}/\partial t]_x = D_{Ox}[\partial^2 C_{Ox}/\partial x^2]_x$$

then the solution of the above via Laplace methods yields [8]

$$(C^{bulk} - C^s) = I_1 / n FSD^{1/2} O_x \text{ and}$$

$$C^{bulk} = I_{lim} / n FSD^{1/2} O_x$$

where  $C^{bulk}$  &  $C^s$  is the bulk and surface concentrations respectively and the convolution  $I_1$  is given by

$$I_1 = i^*(\pi t)^{-1/2} \text{ or more 'fully' as}$$

$$I_1(t) = \pi^{-1/2} \int_0^t i(u) / (t-u)^{1/2} du \quad (2)$$

and  $I_{lim}$  is the limiting value of  $I_1$  at 'extreme' potentials i.e. when the concentration at the electrode  $C^s$  is effectively

reduced to zero by rapid redox conversion and the current is thus controlled solely by the maximum rates of diffusion to (and from) the electrode.

In the case of electron transfer followed by homogeneous decomposition equation (3)



$$(k_1 \gg k_{-1}), (k_c = k_1 + k_{-1})$$

where  $k^0, \alpha, D, E^0, k_1, k_{-1}$  and  $k_c$  are defined as following [10]:

$k^0$  - the standard heterogeneous rate constant

$\alpha$  - the transfer coefficient

$D$  - the diffusion coefficient

$E^0$  - reduction potential

$k_1$  - the forward homogeneous chemical rate constant

$k_{-1}$  - the backward homogeneous chemical rate constant

$k_c$  - the homogeneous chemical rate constant.

The species here are produced by electron transfer at a planar electrode and decomposed in the bulk via a first order chemical reaction of rate constant  $k_c$ . The Fick's Second Law expression is now [9, 10]

$$[\partial C_R/\partial t]_x = D_R[\partial^2 C_R/\partial x^2]_x - k_c C_R(at x)$$

and solution via Laplace methods gives here, necessarily starting at zero concentration in the bulk, the following electrode concentration

$$C^s_R = I_2 / nFAD^{1/2} R$$

where the 'kinetic' convolution  $I_2$  is given by [10]

$$I_2(t) = \pi^{-1/2} \int_0^t [i(u).exp(-k_c(t-u))]/(t-u)^{1/2} du. \quad (4)$$

Thus in the  $I_2$  convolution at time  $t$ , each segment of  $i(u)$  is scaled by dividing by the square root of the time which has elapsed from  $t$  to the time  $u$  to which the segment refers and likewise is scaled by the exponential factor  $exp(-k_c(t-u))$ . Thus  $I_2$  for example now goes to a plateau (at zero) on return of the sweep in cyclic voltammetry and this property allows determination of  $k_c$ .

Several algorithms have been proposed for the evaluation of the convolution integral  $I(t)$ . The following one was used in this work: [11-15]

$$I(t) = \frac{1}{\sqrt{\pi}} \sum_{j=1}^{j=k} \frac{\Gamma(k-j + 1/2)}{(k-j)!} \cdot \Delta t^{1/2} i(j \Delta t) \quad (5)$$

in which  $k$  is the index of the discrete convoluted current being calculated ( $I(k\Delta t)$ ),  $j$  is the series counter to the discrete current data points  $0 \dots k$ ,  $\Delta t$  is the time interval between successive data points, and  $\Gamma(f)$  is the gamma function of  $f$ .

The present work aimed to characterize the nature of the  $EC_{irr}$  scheme (electron transfer followed by fast chemical step) via  $I_{1(end)}$  (convoluted current at the end of the backward sweeps), and the ratio of the height of the forward sweep to the backward one of deconvoluted current  $(di_f/dt)/(di_r/dt)_b$  vs the square root of scan speed  $(v)^{1/2}$  plots. The determination of  $E^0$  and  $k_c$  via accurate and simple convolutive method was carried out and discussed. The selected experimental example for  $EC_{irr}$  is the electroreduction of  $N,N$ -propylene-bis-(salicylideneiminato)Mn(III) complex in phosphate buffer solution at mercury electrode. Digital simulation was combined with experimental work to verify our proposed method for calculating the electrochemical parameters as well as the identification of the nature of the electrode reaction.

## Experimental part

### Materials and apparatus

The investigated  $N,N$ -Propylene-bis-(salicylideneiminato)-Mn(III) complex was prepared according to the method described in the literature [6]. An alcoholic (40% v/v) of the complex in phosphate buffer as supporting electrolyte was tested. The reagents were generally of laboratory grade. Triply distilled mercury was employed. The complex was dissolved in alcoholic phosphate buffer solution ( $pH = 7.4$ ) as supporting electrolyte which proceed at the mercury electrode as  $EC_{irr}$  process [16].

The experimental data were obtained using an electrochemical cell connected to a potentiostat Model 264 PAR (from EG&G). The electrode assembly with a hanging mercury drop electrode (surface area  $2.6 \times 10^{-4} \text{ m}^2$ ) as a working electrode, a platinum wire as auxiliary electrode and a  $Ag/AgCl$  as a reference electrode was used. The auxiliary and reference electrodes were platinum and  $Ag/AgCl$  respectively. The sweep rate in the range from  $0.05$  to  $5 \text{ V s}^{-1}$  were used. Working solutions were degassed thoroughly with oxygen free nitrogen and a nitrogen atmosphere was maintained above the solution throughout the course of measurements.

Convolution-deconvolution voltammetry were performed by Condecon software based on the method established in literature [17, 18]. The digital simulation of the generated cyclic voltammograms was carried out on PC computer using EG & G Condesim package.

## Results and discussion

### Characterization of $EC_{irr}$ system

Figure 1a represent the experimental cyclic voltammogram of  $N,N$ -propylene-bis-(salicylideneiminato) Mn(III) complex in phosphate buffer solution at mercury electrode, scan speed  $5 \text{ V/s}$  and temperature  $298 \text{ K}$ , while figure 1b shows the simulated cyclic voltammogram of  $EC_{irr}$  system at scan speed  $0.2 \text{ V/s}$ ,  $T = 298 \text{ K}$  using the following electrochemical parameters: diffusion coefficient ( $D$ ) =  $5 \times 10^{-9} \text{ m}^2 \text{ s}^{-1}$ , standard heterogeneous rate constant ( $k_c$ ) =  $2 \times 10^{-5} \text{ m s}^{-1}$ , standard reduction potential ( $E^0$ )  $0.5 \text{ V}$ , transfer coefficient ( $\alpha$ ) =  $0.5$ , homogeneous chemical rate constant

( $k_1$ ) =  $19 \text{ s}^{-1}$ , surface electrode area ( $S$ ) =  $2.6 \times 10^{-4} \text{ m}^2$ .

The  $I_1$  convolution of Mn(III) – complex in phosphate buffer solution at sweep rates of  $0.5 \text{ V/s}$  is shown in figure 2. The convoluted current indicates a distinct separation between the forward and reverse sweep and clearly indicates the sluggishness of electron transfer of the electrode process as well as the presence of a fast chemical reaction following the charge transfer. Also it was found that the magnitude of  $I_{1(end)}$  decreases with increasing the sweep rate (i.e. decreasing the duration time of the experiment).

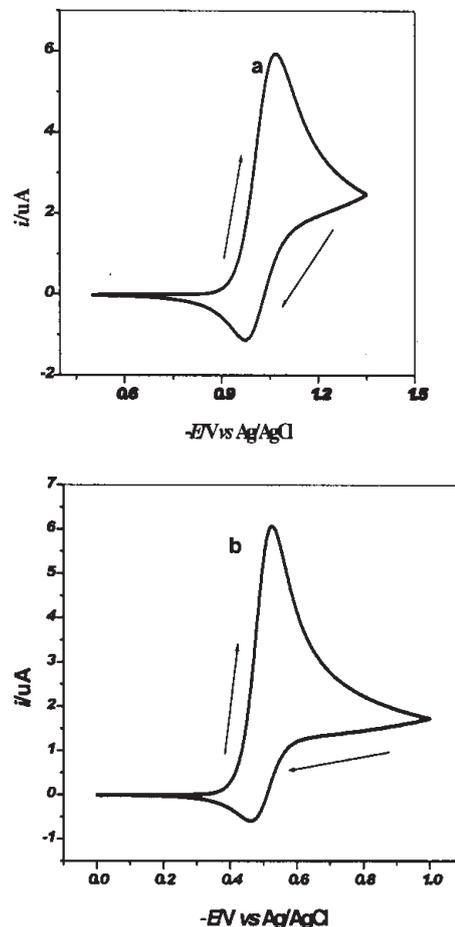


Fig. 1 experimental (a) and Simulated (b) cyclic voltammograms of  $EC_{irr}$  system

The deconvolution of current can be expressed as the differential of the  $I_1$  convolution. In more general terms deconvolution is akin to semi-differentiation in a similar manner to considering  $t^{-1/2}$  convolution as semi-integration.

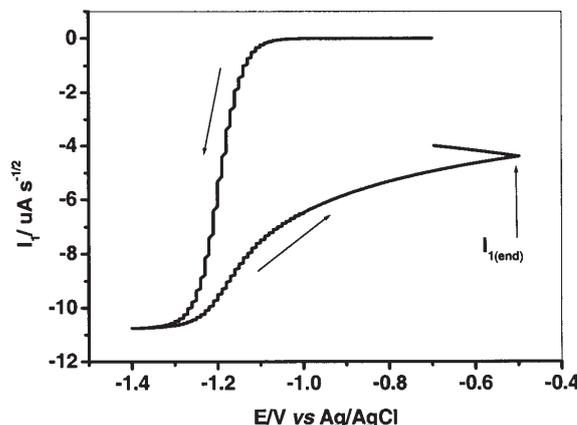
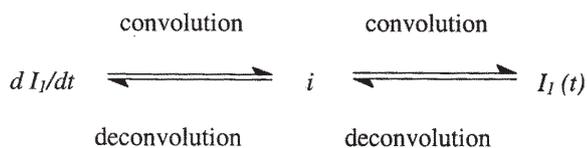


Fig. 2  $I_1$  convolution of Mn(III) – complex in phosphate buffer solution at sweep rates of  $0.5 \text{ V/s}$

The relationship between  $t^{-1/2}$  convolutions and deconvolutions is indicated in the following scheme [10].



The semiderivative (e) of current  $I$  is defined as [19]:

$$e = d^{1/2}i / dt^{1/2} = dI_1/dt$$

which consist of two mirror – image peaks with a maximum and minimum amplitude alignment at  $E_{1/2}$  values and the value of half-width  $w^p$  equals to  $3.526 RT/nF$  or  $90.53/n$  mV in case of rapid electron transfer and  $T = 298$  K. Figure 3 indicates an example of deconvoluted current  $(dI_1/dt)$  of Mn(III) – complex at sweep rate of  $0.5 \text{ V s}^{-1}$  which indicate the non symmetry of the forward and backward sweep confirming the existence of  $EC_{irr}$  nature of the electrode mechanism. It was found that with increasing the sweep rate, the homogeneous chemical rate constant decreases due to the decreasing of the time of

the experiment, i.e. the  $(dI_1/dt)_f / (dI_1/dt)_b$  decrease with increasing the sweep rate.

The plots of the simulated convoluted current at the end of the return sweep,  $I_{1(end)}$ , and the ratio of the simulated forward to backward heights of deconvoluted current  $(dI_1/dt)_f / (dI_1/dt)_b$  versus square root of scan speed  $(v)^{1/2}$  are shown in figure 4. The curves in the plot exhibited that for generated  $EC_{irr}$  the values of  $I_{1(end)}$  and  $(dI_1/dt)_f / (dI_1/dt)_b$  decrease on increasing the square root of sweep rate. The plot of the experimental  $I_{1(end)}$  and  $(dI_1/dt)_f / (dI_1/dt)_b$  versus the square root of sweep rate  $(v)^{1/2}$  are shown in figure 5 which compare well with the trend obtained in figure 4.

*Estimation of the homogeneous chemical rate constant ( $k_c$ ) and the reduction potential ( $E^0$ ) of the  $EC_{irr}$  mechanism*

Equation (3) of  $EC_{irr}$  reaction scheme was treated to give equation (6) [20, 22]:

$$\begin{array}{ccc}
 i(D_{Ox})^{1/2} e^{-\xi} & D_{Ox} & \\
 \text{-----} = I_{lima} - I_1 - I_2 \text{ (-----)}^{1/2} e^{-\xi} & & (6) \\
 k^0 & D_R & 
 \end{array}$$

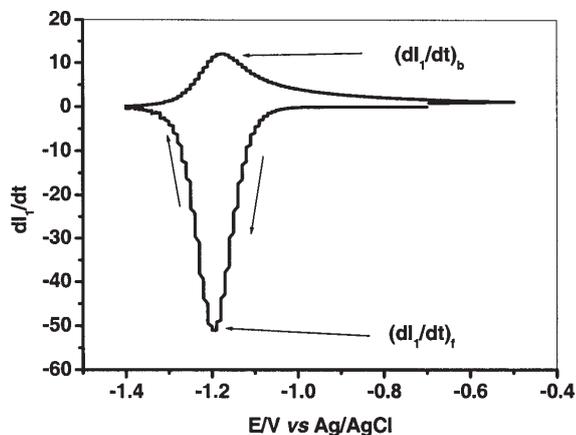


Fig. 3. Deconvolution voltammogram  $(dI_1/dt)$  of Mn(III) – complex in phosphate buffer solution at sweep rates of  $0.5 \text{ Vs}^{-1}$

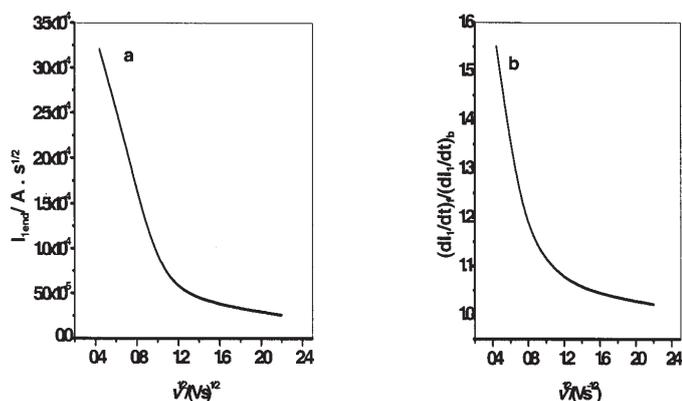


Fig. 4. Simulated  $I_{1(end)}$  (a) and  $(dI_1/dt)_f / (dI_1/dt)_b$  (b) versus square root of sweep rate of  $EC_{irr}$  system

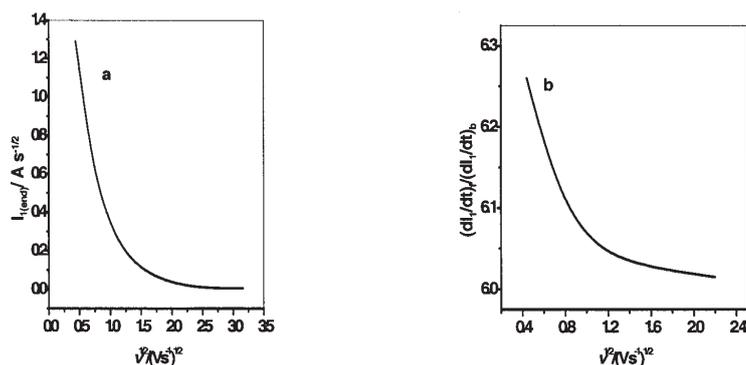


Fig. 5. Experimental  $I_{1(end)}$  (a) and  $(dI_1/dt)_f / (dI_1/dt)_b$  (b) of  $EC_{irr}$  system versus square root of sweep rate

**Table 1**  
EXPERIMENTAL DATA OF  $I_1$  CONVOLUTION, KINETIC CONVOLUTION ( $I_2$ ) AND  $I_{lim} - I_1$  AT VARIOUS VALUES OF POTENTIAL FOR  $EC_{irr}$  SYSTEM (Mn-COMPLEX), at  $k_c = 19 \text{ s}^{-1}$  AND  $\nu = 5 \text{ Vs}^{-1}$

-E/V	$I_1/A \text{ s}^{-1/2}$	$I_2/A \text{ s}^{-1/2}$	$(I_{lim}-I_1)/A \text{ s}^{-1/2}$
0.928	9.607E-8	5.137E-6	2.241E-7
0.979	8.326E-7	4.531E-6	9.607E-7
0.984	9.927E-7	4.426E-6	1.088E-6
1.005	1.665E-6	3.899E-6	1.729E-6
<b>1.020</b>	<b>2.657E-6</b>	<b>2.921E-6</b>	<b>2.921E-6</b>
1.040	3.394E-6	2.188E-6	3.810E-6
1.066	4.570E-6	1.554E-6	4.579E-6
1.080	5.440E-6	9.748E-7	5.280E-6
1.107	5.860E-6	4.470E-7	5.924E-6

where  $I_{lim}$ , and  $\zeta$  are defined as following [7, 19]:

$$I_{lim} \text{ is the limiting convoluted current}$$

$$\zeta = (E - E^0)nF/RT$$

So, on the region  $i = 0$  equation (6) yields

$$I_{lim} = I_1 + I_2(D_A/D_B)^{1/2} \exp(-\zeta)$$

assuming  $(D_A) = (D_B)$  then

$$I_{lim} = I_1 + I_2 \exp(-(E - E^0)(nF/RT))$$

$$I_{lim} - I_1 = I_2 \exp(-(E - E^0)(nF/RT)) \quad (7)$$

So, from equation (7) we can calculate the true value of  $k_c$  and  $E^0$  simultaneously. Example of the computed numerical values of  $I_1$ ,  $I_2$  convolution and  $I_{lim} - I_1$  at various potentials of Mn-complex ( $EC_{irr}$  system) under consideration are listed in table 1, indicating the equality of  $I_{lim} - I_1$  and  $I_2$  at  $E^0$  (-1.02 V) when the value of  $k_c$  true is ( $19 \text{ s}^{-1}$ ). Figure 6a shows the plot of  $I_{lim} - I_1$  and  $I_2$  vs  $E$  of N,N-Propylene-bis-(salicylideneiminato)-Mn(III) complex which proceed as  $EC_{irr}$  mechanism indicates that the curves intersect at standard reduction potential ( $E^0$ ) when  $k_c$  is true. Figure 6b gives example response of  $I_{lim} - I_1$  and  $I_2$  vs  $E$  of theoretical  $EC_{irr}$ .

## Conclusions

In present article we succeeded in applying convolution – deconvolution voltammetry combined with digital simulation method for the characterization and the determination of the relevant chemical and electrochemical parameters of  $EC_{irr}$  scheme. The application of this methods provides the opportunity for obtaining accurate kinetic parameters very precisely irrespective to the rate of charge transfer. The test of the validity of our method is carried out by applying it to the electroreduction of N,N-Propylene-bis-(salicylideneiminato)-Mn(III) complex in phosphate buffer solution at the hanging mercury drop electrode, and is found to give good result confirming the accuracy of the proposed method.

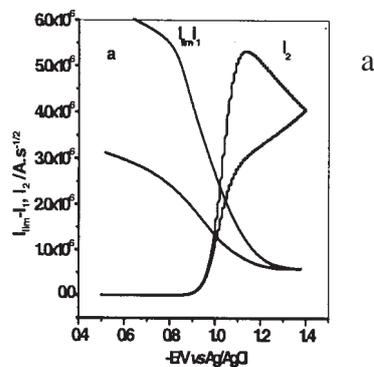
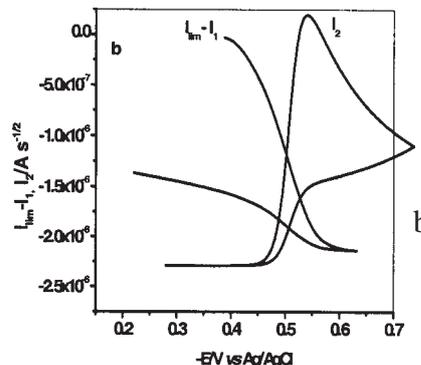


Fig. 6 Experimental  $I_{lim} - I_1$  and  $I_2$  versus the applied potential of the investigated system (a), simulated (b)



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